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STATE-OF-THE-ART IN UNSTEADY AERODYNAMICS, (U)
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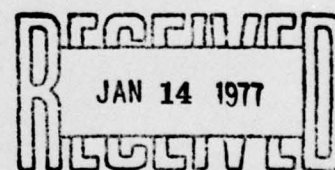
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State-of-the-Art in Unsteady Aerodynamics

by

W.P.Rodden

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AGARD Report No.650

6 STATE-OF-THE-ART IN UNSTEADY AERODYNAMICS

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11 Nov 76

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Paper presented at the 43rd Structures and Materials Panel meeting,
 London, September 1976.

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Published November 1976

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ISBN 92-835-1230-9



*Printed by Technical Editing and Reproduction Ltd
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PREFACE

The accurate prediction of unsteady air loads is essential to avoiding problems and assuring safety in the many interdisciplinary regions involving aeroelasticity and the dynamics of active controls. However, the methods to predict such airloads are complex and intricate. It was considered essential to specify standard configurations and parameters, and to encourage pioneering NATO scientists to report their results early. This would provide bases for evaluation and improvement of later and following developments by other countries. The first cooperative effort involved isolated surfaces in subsonic and supersonic flow, and is reported by D.L.Woodcock in AGARD Report No.583 ("A Comparison of Methods Used in Lifting Surface Theory", 1971). The noticeable success led to another effort on interfering lifting surfaces and is reported by W.P.Rodden in AGARD Report No.643 ("A Comparison of Methods Used in Interfering Lifting Surface Theory", 1976). Both are supplements to the AGARD Manual on Aeroelasticity, Vol.VI. The latter effort and report has also proved to be highly successful.

New developments are rapidly emerging in unsteady aerodynamics. The aeroelastician will continue heavy reliance on prediction of airloads from theoretical methods. A terse description of the new state of the art was required and has been very competently provided by Dr Rodden in this report. The Sub-Committee on Aeroelasticity and Unsteady Aerodynamics will use this framework to establish high priority, cooperative, comparative computational AGARD programs. Transonic and control surface unsteady aerodynamics are likely selection candidates.

W. J. Mykytow

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STATE-OF-THE-ART IN UNSTEADY AERODYNAMICS

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SUMMARY

A brief survey of new developments in unsteady aerodynamics is made as a proposal for establishing another comparative computational AGARD program. Candidate topics include supersonic interference, transonic flow, wing-body interference, control surfaces, rotary loads on T-tails, interference effects of vortex shedding, and rotating blades. A selected bibliography is presented for each topic to illustrate the present state-of-the-art and its near-term future potential.

INTRODUCTION

This paper is a survey of the state-of-the art of unsteady aerodynamics only in a limited sense. The survey is not intended to be a critical evaluation of the references that constitute the current status, but rather to outline areas which may be of general interest to the Structures and Materials Panel so that another comparative computational study might be made similar to those of Woodcock¹ and Rodden² on comparisons of unsteady aerodynamic calculations for isolated and interfering lifting surfaces, respectively.

Recent surveys of research problem areas have been presented by Laschka³ and McCroskey⁴. These discuss more advanced topics than those mentioned here.

Seven problem areas are proposed here and related recent papers are cited. The first six areas concern fixed wing aircraft and the seventh considers the effects of rotation in rotorcraft and turbomachines. The areas suggested for fixed wing aircraft include further supersonic studies, renewed transonic studies, wing-body interference, control surfaces, rotary loads on T-tails, and interference effects of leading- or side-edge vortex shedding.

SUPERSONIC INTERFERENCE

This subject was one of the comparisons in Ref. 2 but only limited calculations by two methods were compared. A large number of new approaches have appeared recently and it would seem reasonable to invite applications of these new methods to some of the standard AGARD configurations. The new methods with which the author is familiar include: the integrated potential formulation of Appa and Jones⁵, the kernel function method of Cunningham⁶, the finite element doublet method of Giesing and Kálmán⁷, the finite element method of Morino, et al.^{8,9}, the doublet-lattice method of Brock and Griffin¹⁰, the constant pressure panel method of Roger¹¹, the modified Mach Box method of Chipman¹², and the characteristic box method of Schmid¹³. There are significant differences among these new approaches and the extent to which computed results by each agreed would add considerably to an improved understanding of supersonic interference.

TRANSONIC FLOW

Sonic calculations by a collocation method were presented in Ref. 1 for isolated wings. Much progress in unsteady transonic flow theory has occurred since the calculations in Ref. 1 were collected. A recent survey by Tijdeman¹⁴ has summarized the significant developments of the past three years. Table 1 of Ref. 14 is reproduced here as Table 1 and the 20 references are also cited here¹⁵⁻³⁴. Most of these works concern two-dimensional airfoils but a few treat the three-dimensional case.

In his concluding remarks, Tijdeman notes "that inserting the effects of thickness, incidence of the airfoil and of shock waves in inviscid theory is an important step forward. However, as shown..., the effect of the boundary layer is of the same order of magnitude and thus of the same importance. Therefore, realistic improvements from the aeroelastician point of view may be expected only if also the second step is made, namely the inclusion of the boundary layer. In this respect the study of the behavior of boundary layers under unsteady flow conditions will become important." The importance of viscous effects has also been observed in hinge moment predictions for control surfaces by Gray and Davies³⁵, and will be discussed below, but it is interesting to note here that thickness, incidence (which may have larger effects than thickness), and viscous effects should be treated together (or all three effects neglected) in achieving experimental correlations.

The variety of new transonic techniques can also be evaluated by establishing new standardized configurations. Two- and three-dimensional configurations might be based on the NACA 64A410 airfoil analyzed so thoroughly by Magnus and Yoshihara^{25,26}, or the NLR 7301 airfoil, which is representative of the new generation of supercritical airfoils, and is currently undergoing extensive testing and analysis. Reynolds numbers as well as Mach numbers should also be selected among the governing parameters.

WING-BODY INTERFERENCE

A survey of wing-body aerodynamic interaction was presented by Ashley and Rodden³⁶ in 1972. A number of advances at subsonic speeds have been made since then. An interference theory has been developed by Giesing et al.³⁷ in which the lifting surfaces are treated by a combination of the Doublet-Lattice Method, Slender Body Theory, and the Method of Images. A panel method for steady flow for general configurations has been developed by Labrujere and Sytsma³⁸. Bennekens, Roos, and Zwaan³⁹ have combined the Doublet-Lattice Method with an unsteady source method for bodies to obtain a general method for oscillating wing/store configurations. Further applications of this new procedure to oscillating wing/body combinations have been made by Roos, et al.⁴⁰. The method of Morino et al.⁴¹ can also be applied to wing-body combinations at both subsonic and supersonic speeds.

A standard configuration for wing-body interference calculations should include a fuselage and an optional store (nacelle)/pylon combination.

CONTROL SURFACES

The accuracy with which potential theory has been observed to predict the loading on interfering lifting surfaces or wing-body combinations decreases toward the trailing edge and the combined effects of thickness and viscosity (see Tijdeman's remarks above under Transonic Flow) probably explain discrepancies with experiment in hinge moment predictions. Accurate hinge moments are necessary to determine power requirements in active control systems for load alleviation and flutter suppression, as well as to predict flutter involving control surface motion. Some of the references cited in the preceding section account for thickness of wings as well as bodies. The additional effects of viscosity via a shear layer have been considered by Dowell, Ventres, and Yates^{41,42,43}. The shear layer is an inviscid approximation to a viscous boundary layer.

ROTARY LOADS ON T-TAILS

The rotary loads are as important in predicting T-tail flutter characteristics as the rotary stability derivatives are in predicting lateral-directional stability and control characteristics of aircraft. Some of these require the ability to predict the spanwise distribution of induced drag of oscillating surfaces. Others require the rolling moments caused by oscillatory yaw and sideslip. The yawing moment induced by steady roll was discussed briefly by Kálmán et al.⁴⁴ and Hancock⁴⁵. An accurate method for predicting spanwise distribution of induced drag in steady subsonic flow has been developed by Lan⁴⁶, and has been extended to the case of oscillatory motion in two-⁴⁷ and three-dimensions⁴⁸. The oscillatory three-dimensional case permits the analysis of ornithopter propulsion⁴⁹ (as well as that of fish and birds!) as well as the oscillatory rotary loads on a T-tail. The oscillatory propulsion of interfering lifting surfaces in two-dimensional flow has also been considered by Bosch⁵⁰.

The problem of spanwise loading and rolling moments caused by oscillatory yawing and sideslipping has been studied by Isogai and Ichikawa⁵¹, but only for incompressible flow.

The rotary aspects of T-tails have not been studied at Mach numbers above subsonic.

The standard AGARD T-tail configuration can provide a basis for comparison of calculated rotary loads.

INTERFERENCE EFFECTS OF VORTEX SHEDDING

Recent interest has been shown regarding the effects on steady loads and flutter of the leading-edge vortex separation from a highly-swept leading edge of either the delta or the swing-wing configuration. This is a nonlinear problem in the flow field geometry. Recent progress in predicting steady loads at subsonic speeds by panel and lattice methods has been made by Brune, et al.⁵² and by Kandil, et al.⁵³ and a very complete bibliography is contained in Ref. 53. The unsteady subsonic case is currently under investigation.

The interference between wing-tip vortices and/or wing jet-flap wakes and horizontal tail load distributions has also attracted recent attention. The steady flow problem at subsonic speeds has been investigated by Goldhammer et al.⁵⁴ and by Shollenberger⁵⁵. Extensions to unsteady flow are also under investigation^{56,57}. Becker's investigation⁵⁷ of slender wing-tail configurations gave good correlation between prediction and measurement, but the predicted airforces were usually high.

The existing standard AGARD configurations are adequate for comparison of calculated nonlinear wake interference effects, although a horizontal tail with a smaller span than the wing might be a more practical configuration.

ROTATING BLADES

Significant progress has been made in adapting lifting surface theories to predict the loading of helicopter rotors. References 27, 28, 58-63 present various approaches and applications that all show promise as a replacement for Strip Theory. Numerical comparisons would appear to be timely in view of the importance of the helicopter in V-STOL Technology.

The Proceedings of a Workshop on Aeroelasticity in Turbomachines⁶⁴ indicates that the cascade problem is only being analyzed by two-dimensional methods. Recent developments in subsonic cascade theory for staggered compressor rotor blades have been made by Rao and Jones⁶⁵ and by Jones and Moore⁶⁶. New solutions for supersonic cascades have been obtained by Verdon and McCune⁶⁷ and by Yates⁶⁸.

CONCLUDING REMARKS

A brief survey has been presented that illustrates a number of new aspects and refinements that have been made recently in unsteady aerodynamics for interfering configurations. Each topic is not only an interesting problem in its own right, but also is an important part of the whole problem of aerodynamic configurations, and the analysis of each has achieved a reasonable level of sophistication. This level of sophistication suggests that a program of comparing calculated results is feasible and could be a profitable experience for the contributors and beneficial to members of AGARD, in the same way that Refs. 1 and 2 have been useful.

Configurations and parameters would have to be agreed upon. A further study of supersonic interference among lifting surfaces requires no new configurations. Transonic flow studies would require a definition of thickness distributions; the NLR 7301 airfoil would be a good choice. The viscous aspects of transonic flow would require Reynolds numbers to be specified. Wing-body interference studies require a fuselage to be defined; at least one additional external-store/pylon configuration should also be considered. Control surface studies would require the planform description in addition to the airfoil thickness and Reynolds numbers; a definition of gaps and seals might also be considered. Rotary effects on T-tails can be calculated for the existing standard AGARD configuration, and calculations of vortex shedding characteristics can also be made on the existing standard configurations. Finally, studies of rotor blade loading would require a standard AGARD rotor blade along with its tip Mach number, advance ratio, and related parameters.

It is hoped that some of the above topics can become the basis of a third AGARD comparative study of computed results. The reference list presented here is only meant to be representative of the state-of-the-art; the author apologizes to the Panel for its American flavor.

ACKNOWLEDGEMENTS

The author wishes to thank Dr. B. Laschka of MBB and H. Tijdeman of NLR for reviewing the manuscript and adding a number of significant references.

Table 1

Review of Calculation Methods for Unsteady Transonic Flow

	Author	Year	Ref.	Remarks
Two-dimensional methods	Stahara and Spreiter	1973	15	{ M ≈ 1.0 no shock waves
	Isogai	1974	16,17	
	Dowell	1975	18	
	Revell	1973	19	layered-medium
	Ehlers	1973	20	finite difference
	Beam and Warming	1974	21	finite difference
	Ballhaus and Lomax	1974	22	finite difference
	Chan and Brashears	1974	23	finite element
	Traci, Farr, Albano & Cheng	1974	24	finite difference
	Magnus and Yoshihara	1975	25,26	finite difference
	Isom and Caradonna	1975	27,28	finite difference
Three-dimensional methods	Ruo and Theisen	1973	29	{ M ≈ 1.0 no shock waves
	Isogai	1974	17	
	Cunningham	1973	30-32	mixed subsonic-supersonic method
	Garner	1975	33	semi-empirical
	Isom and Caradonna	1975	27,28	finite difference
	Weatherhill, Ehlers and Sebastian	1975	34	finite difference

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REPORT DOCUMENTATION PAGE			
1. Recipient's Reference	2. Originator's Reference AGARD-R-650	3. Further Reference ISBN 92-835-1230-9	4. Security Classification of Document UNCLASSIFIED
5. Originator	Advisory Group for Aerospace Research and Development North Atlantic Treaty Organization 7 rue Ancelle, 92200 Neuilly sur Seine, France		
6. Title	STATE-OF-THE-ART IN UNSTEADY AERODYNAMICS		
7. Presented at	the 43rd Structures and Materials Panel meeting, London, September 1976.		
8. Author(s) W.P. Rodden	9. Date November 1976		
10. Author's Address Consulting Engineer 255 Starlight Crest Drive La Canada, California 91011, USA	11. Pages 12		
12. Distribution Statement	This document is distributed in accordance with AGARD policies and regulations, which are outlined on the Outside Back Covers of all AGARD publications.		
13. Keywords/Descriptors	<div style="display: flex; justify-content: space-between;"> <div> Reviews Aerodynamic loads Unsteady flow </div> <div> Aeroelasticity Lifting bodies Mathematical prediction </div> </div>		
14. Abstract <p>→ The accurate prediction of unsteady air loads is essential to avoiding problems and assuring safety in the many interdisciplinary regions involving aeroelasticity and the dynamics of active controls. However, the methods to predict such airloads are complex and intricate. It was considered essential to specify standard configurations and parameters, and to encourage pioneering NATO scientists to report their results early. This would provide bases for evaluation and improvement of later and following developments by other countries. The first co-operative effort involved isolated surfaces in subsonic and supersonic flow, and is reported by D.L. Woodcock in AGARD Report No. 583 ("A Comparison of Methods Used in Lifting Surface Theory", 1971). The noticeable success led to another effort on interfering lifting surfaces and is reported by W.P. Rodden in AGARD Report No. 643 ("A Comparison of Methods Used in Interfering Lifting Surface Theory", 1976). Both are supplements to the AGARD Manual on Aeroelasticity, Vol. VI. The latter effort and report has also proved to be highly successful.</p> <p>→ New developments are rapidly emerging in unsteady aerodynamics. The aeroelastician will continue heavy reliance on prediction of airloads from theoretical methods. A terse description of the new state of the art was required and has been very competently provided by Dr Rodden in this report.</p>			

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